

International Journal of Applied Information Technology



http://journals.telkomuniversity.ac.id/ijait/

Development of Meandered Microstrip Antenna for RFID Application

Vista Agus Sria Warman a, Radial Anwar b,*, Yuyu Wahyu c

- ^{a,b} School of Applied Science, Telkom University, Bandung, Indonesia
- ^c Research Center for Electronics and Telecommunication Indonesia Institute of Sciences, Bandung, Indonesia beivagsva@gmail.com, radialanwar@tass.telkomuniversity.ac.id, yuyu@ppet.lipi.go.id

ARTICLE INFO

Received 05 June 2018 Revised 09 August 2018 Accepted 15 August 2018 Available online 22 December 2018

Keywords microstrip antenna, miniaturization, RFID, meandering

ABSTRACT

Antenna miniaturization has become one important research, especially in mobile communication technology development. This paper presents the development of a miniaturized antenna for RFID application (924 MHz). Meandering technique has been adopted to create a geometrically small antenna relative to its operating frequency. Measurement result shows that the fabricated antenna inherits low return loss, down to -25.915 dB. The geometry of the antenna is 25.54 mm \times 16 mm, which is much smaller than its resonance wavelength (0.079 λ × 0.049 λ). The measured gain is relatively small, of about -12 dBi. Nevertheless, the obtained parameters are acceptable since the antenna is meant for near field communication application.

* Corresponding author at: School of Applied Science, Telkom University, Jl. Telekomunikasi No. 1, Terusan Buah Batu, Bandung, 40257 Indonesia.

 $E-mail\ address: radial anwar@tass.telkomuniversity.ac.id\\$

ORCID ID:

Second Author: 0000-0002-2022-7195

1. Introduction

Mobile communication nowadays requires small, light-weight and low-profile antenna as the front-end sub-system component, especially for near field communication (NFC) application. Therefore, miniaturization of the antenna becomes more explored to obtain geometrically small antennas. Research on this particular field includes the utilization of spiral antennas [1]-[8], miniaturization of PIFA antennas [9]-[10], employment of chip antenna [11] and exploration on material for antenna structure for example magnetic composite films [12].

In RFID application, microstrip patch antenna still one of the most explored antennae, as it not only provides all of the requirements for NFC application but also allows planar installation. Among research in microstrip RFID antenna include printed folded dipole [13], circular loop structure [14] as well as single-sided meandered-dual-antenna structure [15].

This paper presents the development of a miniaturized microstrip patch antenna for RFID application, operated at 924 MHz. This frequency is allocated for RFID application in Indonesia [16] with a bandwidth of 2 MHz. The proposed antenna is meandered by adopting a square loop structure. This method has successfully provided the design of a very small antenna with good return loss.

2. Antenna Architectures

The overall size of the proposed antenna geometry is $25.54~\text{mm} \times 16~\text{mm}$, which is equal to $0.079\lambda \times 0.049\lambda$. Cooper is utilized as the material for the patch and ground plane, with a thickness of 0.035~mm. These patch and ground plane are printed on a 1.6~mm thick FR4 substrate. The patch is using square loop structure with three turns on its loop, separated of about 0.78~mm between loops. The width of the radiating element is 1~mm. The patch is fed using a microstrip line with a length of 13.94~mm from the terminal point and width of 2.9435~mm. On the back side, the ground plane is only 4~mm long from the terminal point, leaving most of the substrate exposed. The geometry of the proposed antenna is shown in Figure 1 while its parameters are listed in Table 1.

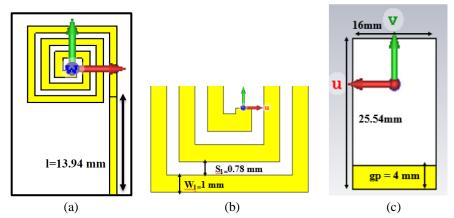


Figure 1 Geometry of the proposed antenna (a); Front-view (b); Detail on the square-loop patch structure (c) back-view

Table 1 Parameter of the proposed antenna geometry

Parameter	Values (mm)
Cooper thickness (patch & ground plane)	0.035
Substrate thickness (FR4)	1.6
Loop separation (S ₁)	0.78 (0.0024λ)
Patch width (W _I)	1 (0.0031λ)
Length of the feeder (l)	13.94 (0.0429λ)
Width of the feeder	2.9435 (0.0091λ)
The Height of the ground plane (gp)	4 (0.0123λ)
Overall length (u)	25.54 (0.079λ)
Overall width (v)	16 (0.049λ)

3. Result and Discussion

Optimization of the antenna overall size is listed in Table 2. It can be seen that the geometry of $25.54 \, \text{mm} \times 16 \, \text{mm}$ provides the center operating frequency at 924 MHz. This center frequency is also affected by the length of the feeder and the height of the ground plane, as shown in Table 3 and 4 respectively.

Table 2 Optimization on the overall size of the proposed antenna

Length (mm)	Width (mm)	Frequency (MHz)
24	15	917
24	16	912
24	17	903
25	15	940
25	16	932
25	17	918
26	15	931
26	16	919
26	17	910
25.54	16	924

 $\textbf{Table 3} \ \textbf{Optimization} \ \textbf{on the length of antenna feeder}$

Those of the section of the section of the section				
Feeder Length (mm)	Peak Frequency	Peak Return		
	(MHz)	Loss (dB)		
6.2	865	-6,931		
7.4	898	-9,998		
11.24	919	-15,98		
12.44	922	-19,71		
13.94	924	-23,96		

Table 4 Optimization on the height of antenna groundplane

Groundplane Height	Peak Frequency	Peak Return
(mm)	(MHz)	Loss (dB)
10	892	-6,46
8	910	-10,196
7	915	-12,118
5	922	-18,424
4	924	-23,968

The return loss of the proposed antenna is also affected by the separation of the loop (S_1) and width of the microstrip patch (W_1) . From Figure 2 and 3, it can be seen that separation of 0.78 mm and patch width of 1 mm provide the lowest return loss.

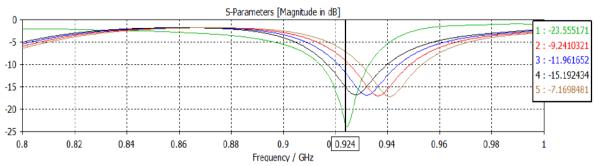


Figure 2 Variation of loop separation on the return loss 1: 0.78 mm. 2: 0.77 mm. 3: 0.76 mm. 4: 0.75 mm. 5: 0.74 mm.

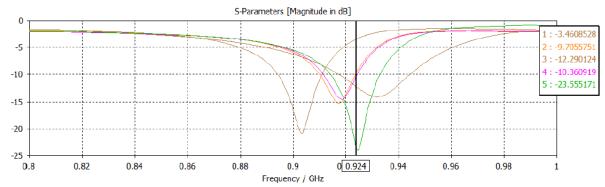


Figure 3 Variation of microstrip patch width on the return loss 1: 0.6 mm. 2: 0.77 mm. 3: 0.8 mm. 4: 0.82 mm. 5: 1 mm.

The proposed antenna has been fabricated and measured. Figure 4 shows the fabricated antenna. It can be seen that the proposed antenna is very small considering its operating frequency.

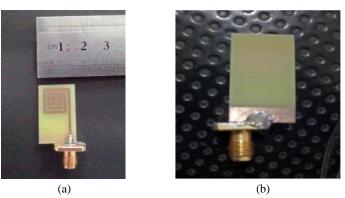


Figure 4 The fabricated antenna; Top view (a); Back view (b)

Figure 5 depicts the snapshot of return loss measurement. The low return loss of about -25.915 dB has been obtained and it is lower than the simulated result (-23.96 dB). The obtained bandwidth is of about 24.6 MHz (2.66%) which as much wider than the requirement for RFID antenna specification.



Figure 5 Measurement of the proposed antenna return loss.

Far-field parameters of the proposed antenna have also been measured. The radiation pattern of the proposed antenna is shown in Figure 6. It can be seen that the measured patterns in azimuth and elevation direction are about the same with the simulated curves, despite the difference in magnitude level. These differences occurred probably due to un-ideal measurement environment, as the antenna was measured not inside an anechoic chamber. The measured gain is about -12 dBi, which is lower than the simulated result, about -10 dB. The polarization has also been measured. The obtained axial ratio is about 5.7263, which is corresponding to elliptical polarization.

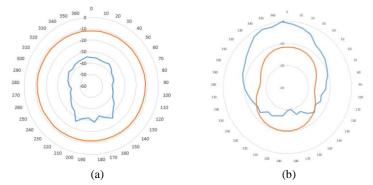


Figure 6 Radiation pattern of the proposed antenna (a) Azimuth (b) Elevation

Simulated Measured

4. Conclusion

Design of a miniaturized RFID antenna has been presented in this paper. The miniaturization was conducted by adopting meandering technique with square loop

structure for the antenna basic geometry. A very small antenna with maximum geometry of $0.079\lambda \times 0.049\lambda$ has been achieved. The obtained antenna inherits low return loss, of about -25.915 dB, with measured bandwidth of about 24.6 MHz. The achieved gain is relatively low, of about -12 dB. Nevertheless, this shortcoming is acceptable considering the application of the proposed antenna, which is meant for near field communication.

Bibliography

- [1] W. Fu, E. R. Lopez, W. S. T. Rowe and K. Ghorbani, "A Planar Dual-Arm Equiangular Spiral Antenna," in *IEEE Transactions on Antennas and Propagation*, vol. 58, no. 5, pp. 1775-1779, May 2010.
- [2] J. M. O'Brien, J. E. Grandfield, G. Mumcu, and T. M. Weller, "Miniaturization of a spiral antenna using periodic Z-Plane meandering," *IEEE Trans. Antennas Propag.*, vol. 63, no. 4, pp. 1843-1848, Apr. 2015.
- [3] N. Rahman, and M. N. Afsar, "A novel modified Archimedean polygonal spiral antenna," *IEEE Trans. Antennas Propag.*, vol. 61, no. 1, pp. 54-61, Jan. 2013.
- [4] Y. W. Zhong, G. M. Yang, J. Y. Mo and L. R. Zheng, "Compact Circularly Polarized Archimedean Spiral Antenna for Ultrawideband Communication Applications," in *IEEE Antennas and Wireless Propagation Letters*, vol. 16, pp. 129-132, 2017.
- [5] K. Nakajima, K. Kunishige, F. Kuroki, Y. Hamada and M. Numoto, "Low-profile and small-sized spiral-shaped microstrip line antenna with multi-band operation in UHF frequency band," 2017 *IEEE Radio and Wireless Symposium (RWS)*, Phoenix, AZ, 2017, pp. 59-61.
- [6] X. Zhang, Y. Han, W. Li, and X. Duan, "A Rectangular Planar Spiral Antenna for GIS Partial Discharge Detection," *International Journal of Antennas and Propagation*, vol. 2014, Article ID 985697, 7 pages, 2014.
- [7] R. Vivek and P.N. Sanket, "Design of Planar Archimedean Spiral Antenna for Wi-Max Using Different Materials," *International Journal of engineering Development* and Research, vol. 2, Issue 2, 2014.
- [8] J. Kracek, M. Svanda, M. Mazanek and J. Machac, "Semi-active 866 MHz RFID implantable tag fed by 6.78 MHz inductive wireless power transfer," 2016 46th European Microwave Conference (EuMC), London, 2016, pp. 620-622.
- [9] M. K. Hosain, A. Z. Kouzani, S. Tye, K. Walder and L. Kong, "Design of a miniature UHF PIFA for DBS implants, "2012 ICME International Conference on Complex Medical Engineering (CME), Kobe, 2012, pp. 485-489.
- [10] A. Munir, A. Harish and Chairunnisa, "Size reduction of UHF planar inverted-F antenna with patch geometry modification," 2014 International Symposium on Antennas and Propagation Conference Proceedings, Kaohsiung, 2014, pp. 537-538.
- [11] A. Zhao and F. Ai, "Dual-Resonance NFC Antenna System Based on NFC Chip Antenna," *IEEE Antennas and Wireless Propagation Letters*, vol. 16, pp. 2856-2860, 2017.
- [12] B. Zhan, D. Su, S. Liu, and F. Liu, "Wearable near-field communication antennas with magnetic composite films," *AIP Advances* 7, 065313, 2017.
- [13] S.-L. Chen and K.-H. Lin, "A folded dipole with a close loop antenna for RFID applications," in *Proc. IEEE AP-S Int. Symp. and URSI Radio Science Meeting, Honolulu*, HI, Jun. 2007, pp. 2281–2284.
- [14] H.-K. Ryu and J.-M. Woo, "Size reduction in UHF band RFID tag antenna based on circular loop antenna," in *Proc. 18th Int. Conf. on Applied Electromagnetics and Communications*, Oct. 2005, pp. 1–4.
- [15] P. Kamalvand, G. K. Pandey, and M. K. Meshram, "A single-sided meandered-dual-antenna structure for UHF RFID tags," *International Journal of Microwave and Wireless Technologies*, vol. 9, no. 7, pp. 1419–1426, 2017.
- [16] Directorate General of Telecommunications, Indonesia. Regulation No. 34, 2012. Available: http://www.postel.go.id/downloads/40/20130128134001-PM-34-2012.pdf [Accessed on 4 June 2018]